


**Series of exercises 5 - Constitutive equations for simple models of continuum**

1. **Example 1** Uma camada de água escorrega, devido a acção do seu peso, por um plano inclinado de inclinação  $\alpha = 30^\circ$  e de altura  $h = 0,5\text{ m}$ . Figura 5.1.1. A corrente de água está limitada pelas paredes laterais e a distância entre as paredes (a largura de escoamento) é  $a = 10\text{ cm}$ . A taxa volémica de escoamento é  $G = 21/\text{s}$ . A pressão fora da água é atmosférica,  $p = p_0$ , a espessura da camada no topo do plano  $\delta_0 = 1\text{ cm}$ . Despreze a viscosidade da água. Encontre os seguintes parâmetros no ponto mais baixo (saída) do plano: a velocidade de água, a espessura da camada, a pressão exercida pela água sobre o plano.
2. If the Lame constants for a material are:  $\lambda = 119,2\text{ GPa}$ ;  $\mu = 79,2\text{ GPa}$ , find Young's modulus, Poisson's ratio, and the bulk modulus.
3. Given Young's modulus  $E_Y = 193\text{ GPa}$  and shear modulus  $\mu = 76\text{ GPa}$ , find Poisson's ratio  $\nu$ , Lame's constant  $\lambda$  and the bulk modulus  $k$ .
4. If the components of strain at a point of structural steel are:  $E_{11} = 100 \times 10^{-6}$ ,  $E_{22} = -50 \times 10^{-6}$ ,  $E_{33} = 200 \times 10^{-6}$ ,  $E_{12} = -100 \times 10^{-6}$ ,  $E_{23} = 0$ ,  $E_{13} = 0$ . find the stress components ( $\lambda = 119,2\text{ GPa}$ ;  $\mu = 79,2\text{ GPa}$ ).
5. Consider the constant stress field below

$$\begin{bmatrix} \hat{T} \end{bmatrix} = \begin{bmatrix} 6 & 2 & 0 \\ 2 & -3 & 0 \\ 0 & 0 & 0 \end{bmatrix} \text{ MPa}$$

Use the elastic constants  $\mu = 79,2\text{ GPa}$ ,  $\nu = 0,30$ :

- (a) Find the strain components.
- (b) Suppose that a sphere of  $5\text{ cm}$  radius is under the influence of this stress field, what will be the change in volume of the sphere?
6. **Example 5** Given the following velocity field:

$$v_1 = -k(x_1 + x_2), \quad v_2 = k(x_2 - x_1), \quad v_3 = 0, \quad k = 1\text{ s}^{-1}$$

for a Newtonian liquid with viscosity,  $\mu = 10^{-3}\text{ Pa} \cdot \text{s}$ . For a plane whose normal is in the  $\mathbf{e}_1$ -direction.

- (a) Find the excess of the total normal compressive stress over the pressure  $p$
- (b) Find the magnitude of the shearing stress.
7. Given the following velocity field in  $\text{m s}^{-1}$  for a newtonian incompressible fluid with a viscosity  $\mu = 0.96\text{ mPa}$ :

$$v_1 = x_1^2 - x_2^2; \quad v_2 = -2x_1x_2; \quad v_3 = 0$$

At the point  $(1, 2, 1)\text{ m}$  and on the plane whose normal is in the direction of  $\mathbf{e}_1$ :

- (a) find the excess of the total normal compressive stress over the pressure  $p$ ,
- (b) find the magnitude of the shearing stress.

8. Given the velocity field of a linearly viscous fluid

$$v_1 = kx_1, \quad v_2 = -kx_2, \quad v_3 = 0$$

- (a) Show that the velocity field is irrotational.
- (b) Find the stress tensor.
- (c) Find the acceleration field.
- (d) Show that the velocity field satisfies the Navier-Stokes equations by finding the pressure distribution directly from the equations. Neglect body forces. Take  $p = p_0$  at the origin.

9. Repeat the preceding exercise for the following velocity field:

$$v_1 = k(x_1^2 - x_2^2), \quad v_2 = -2kx_1x_2, \quad v_3 = 0$$

10. Show that for the velocity field

$$v_1 = v(y, z), \quad v_2 = v_3 = 0$$

the Navier-Stokes equations, with  $\rho\mathbf{B} = \mathbf{0}$ , reduces to

$$\frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} = \frac{1}{\mu} \frac{dp}{dx}$$

11. **Example 6** Determine the general form of the stress tensor for an unidimensional flow  $\mathbf{v} = (v_1, 0, 0)$  of an incompressible fluid.

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### Solutions:

- 1)  $v_1 = \sqrt{v_0^2 + 2gx_1 \sin \alpha} = 3.7 \frac{\text{m}}{\text{s}}$ ;  $\delta = \frac{G}{av_1} = 5.4 \text{ mm}$ ;  $p|_{x_2=0, x_1 \sin \alpha = h} = p_0 + \delta \rho g \cos \alpha \approx 1 \text{ bar}$ ;
- 2)  $E_Y = 207 \text{ GPa}$ ;  $\nu = 0, 30$ ;  $k = 172 \text{ GPa}$ ; 3)  $\nu = 0, 27$ ;  $\lambda = 89 \text{ GPa}$ ;  $k = 140 \text{ GPa}$ ; 4)  $\begin{bmatrix} \widehat{T} \end{bmatrix} = \begin{bmatrix} 45640 & -15840 & 0 \\ -15840 & 21880 & 0 \\ 0 & 0 & 61480 \end{bmatrix} \times 10^3 \text{ Pa}$ ; 5a)  $\begin{bmatrix} \widehat{E} \end{bmatrix} = \begin{bmatrix} 3,34 & 1,26 & 0 \\ 1,26 & -2,33 & 0 \\ 0 & 0 & -0,44 \end{bmatrix} \times 10^{-5}$ ; b)  $\Delta V = 3 \times 10^{-3} \text{ cm}^3$ ;
- 6.a)  $-T_{11} - p = 2\mu k = 2 \cdot 10^{-3} \text{ Pa}$ ; b)  $T_{21} = -2\mu k = -2 \cdot 10^{-3} \text{ Pa}$ ;  $T_{31} = 2\mu D_{31} = 0$ ; 7a)  $-4\mu = -3,84 \times 10^{-3} \text{ Pa}$ ; b)  $T_{21} = -8\mu \text{ Pa} = -7,68 \times 10^{-3} \text{ Pa}$ ;  $T_{31} = 0 \text{ Pa}$ ; 8b)  $\begin{bmatrix} \widehat{T} \end{bmatrix} = \begin{bmatrix} -p + 2\mu k & 0 & 0 \\ 0 & -p - 2\mu k & 0 \\ 0 & 0 & -p \end{bmatrix}$ ;
- c)  $\mathbf{a} = k^2(x_1, x_2, 0)$ ; d)  $p = p_0 - \frac{\rho k^2}{2}(x_1^2 + x_2^2)$ ; 9b)  $\begin{bmatrix} \widehat{T} \end{bmatrix} = \begin{bmatrix} -p + 4\mu k x_1 & -4\mu k x_2 & 0 \\ -4\mu k x_2 & -p - 4\mu k x_1 & 0 \\ 0 & 0 & -p \end{bmatrix}$ ; c)  $\mathbf{a} = 2k^2(x_1^3 + 2x_1 x_2^2, x_1^2 x_2 + x_2^3, 0)$ ; d)  $p = p_0 - 2\rho k^2 \left( \frac{x_1^4}{4} + \frac{x_2^4}{4} \right)$ ; 11)  $\begin{bmatrix} \widehat{T} \end{bmatrix} = \begin{bmatrix} -p & \mu \frac{\partial v_1}{\partial x_2} & \mu \frac{\partial v_1}{\partial x_3} \\ \mu \frac{\partial v_1}{\partial x_2} & -p & 0 \\ \mu \frac{\partial v_1}{\partial x_3} & 0 & -p \end{bmatrix}$ .